



3D Numerical simulation of solidification of large size ingots of high strength steels

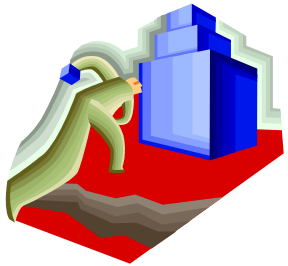
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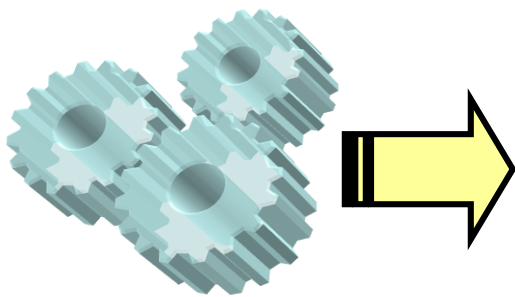




▪ Objectives Of This Research

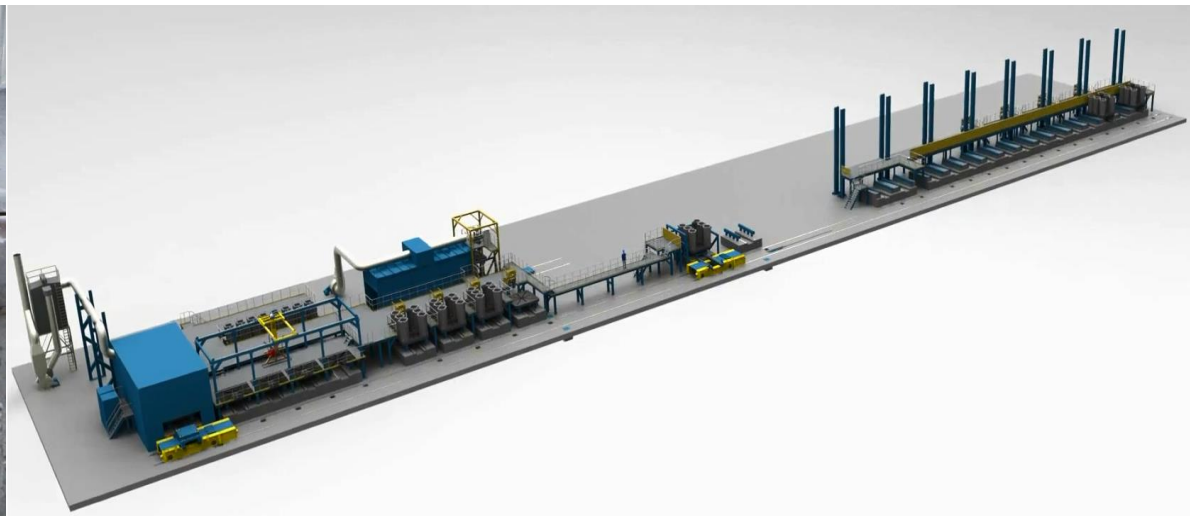
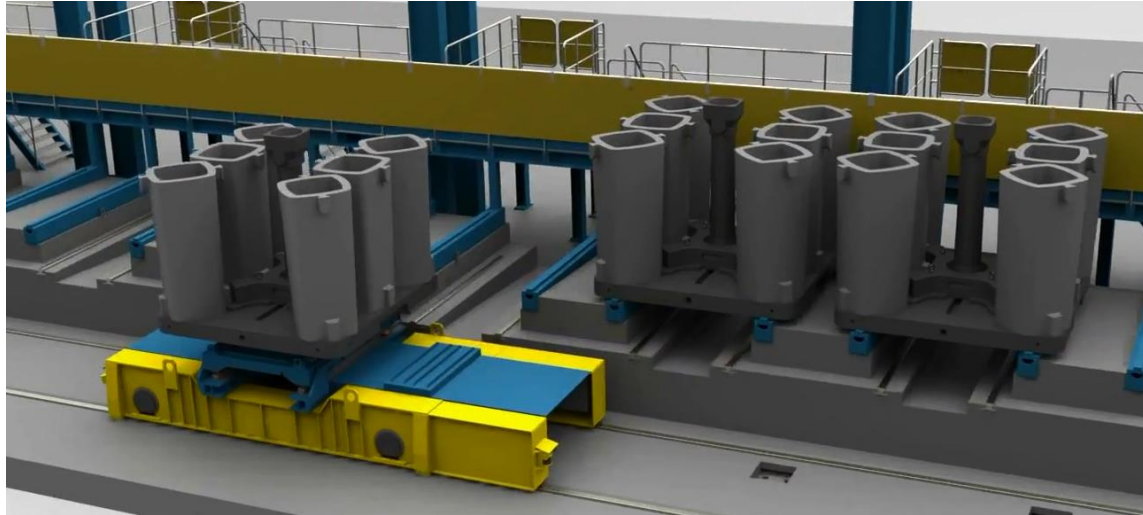
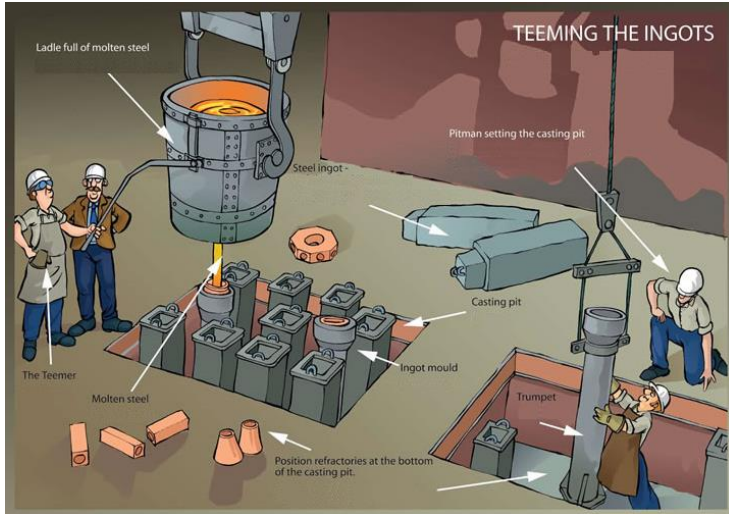


- Numerical Simulation and Equations for Ingot Casting
- Flow of Steps Involved in the Large Ingot Solidification
- Factors Affecting Solidification Time
- Material Properties, Geometrical & Computational Model



- Setup for Computing Time
- Empirical Model for Solidification Time
- Results and Discussion
- Experimental Validation
- Conclusions

Objective of the Research

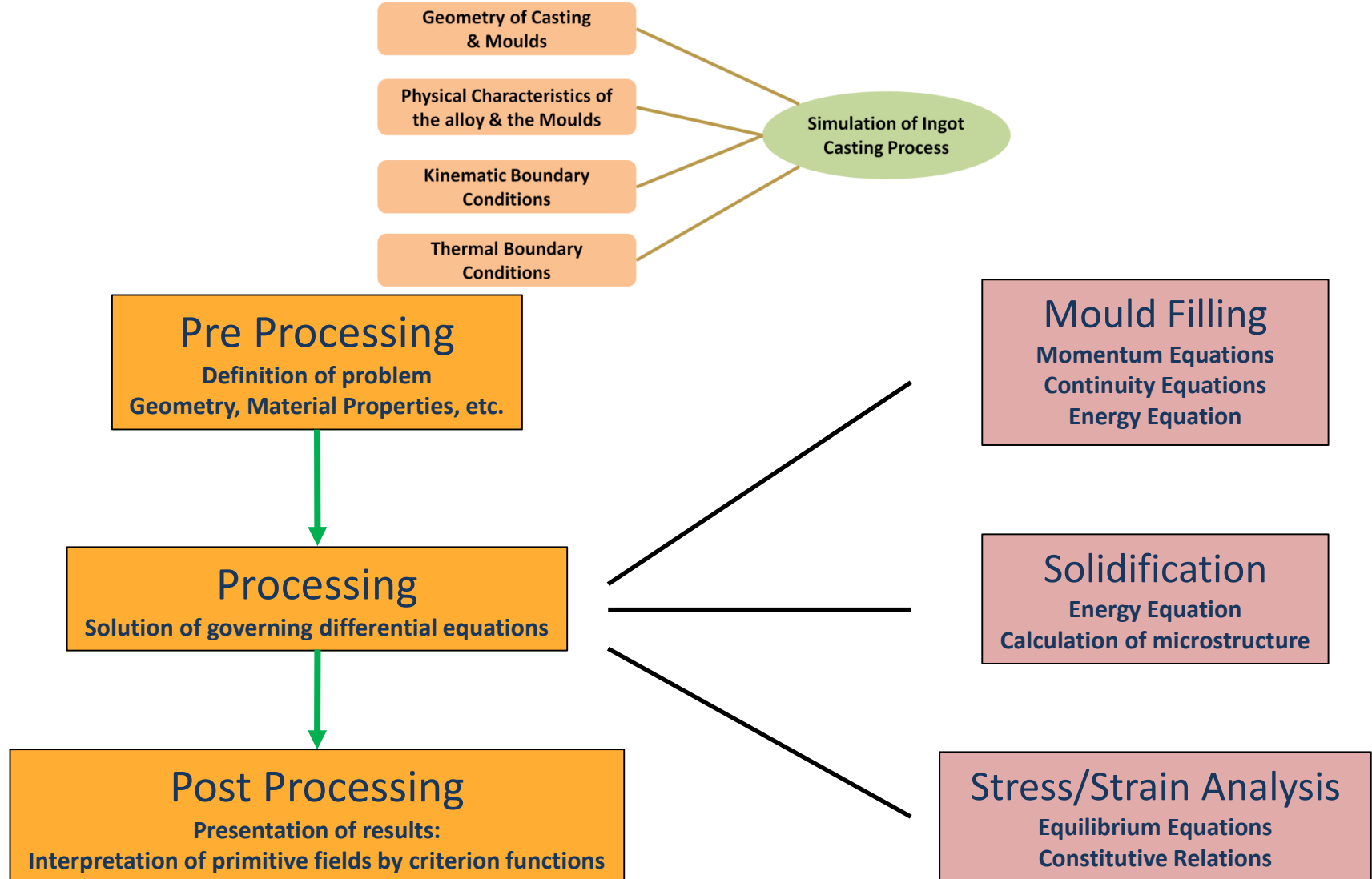


- 1) www.wrexham.gov.uk
- 2) www.svpt.se
- 3) www.sorelforge.com

✓ Effects of Casting Parameters on Solidification Time of Large Size Ingot of High Strength Steels using Numerical Simulation

D. Shahriari, A. Loucif, M. Jahazi, R. Tremblay and R. Beauvais -ÉTS (Sept. 25, 2015)

□ Concept of Numerical Simulation for Ingot Casting



❑ Basic Equations in Ingot Casting Simulation-Methodology for Numerical Tool Selection

➤ Momentum Equations

Navier–Stokes equations (general)

$$\rho \left(\frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} \right) = -\nabla p + \nabla \cdot \mathbf{T} + \mathbf{f}$$

V: flow velocity

ρ: fluid Density

P: Pressure

T: deviatoric components (stress tensor)

f: body force

$$\nabla = \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right) = \hat{\mathbf{x}} \frac{\partial}{\partial x} + \hat{\mathbf{y}} \frac{\partial}{\partial y} + \hat{\mathbf{z}} \frac{\partial}{\partial z}$$

➤ Continuity Equations in Fluid Dynamic

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0 \quad \mathbf{u}: \text{flow velocity}$$

✓ Heat Equation

➤ Continuity Equations for Energy Flow

$$\frac{\partial u}{\partial t} + \nabla \cdot \mathbf{q} = 0 \quad \begin{array}{l} u: \text{energy density} \\ \mathbf{q}: \text{energy flux} \end{array} \quad \longrightarrow \quad \frac{\partial T}{\partial t} = \alpha \nabla^2 T$$

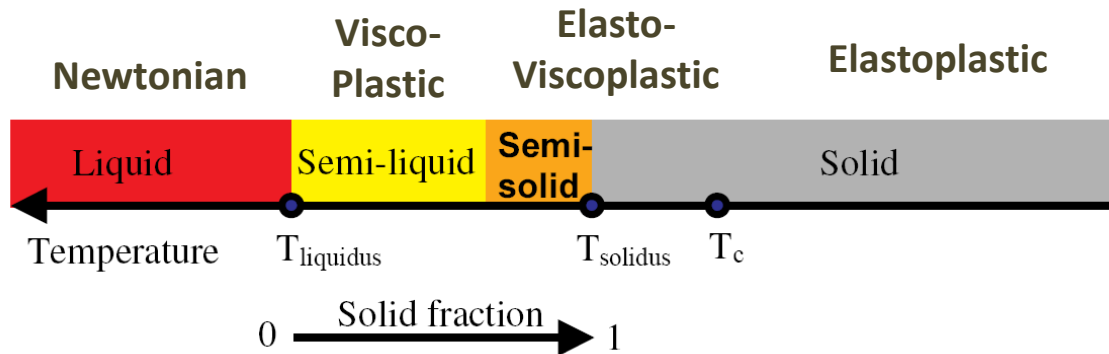
1) J.N. Reddy, *An Introduction to Continuum Mechanics With Applications*, Cambridge University Press, 2008.

2) P.M. Dixit, U.S. Dixit, *Plasticity Fundamentals and Applications*, CRC Press, Taylor & Francis Group, 2015.

3) U.S., Dixit, S. Joshi, S. N., and J.P. Davim, *Incorporation of material behavior in modeling of metal forming and machining processes: A review*, *Materials & Design*, Vol. 32, 2011, pp. 3655–3670.

Basic Equations in Ingot Casting Simulation-Methodology for Numerical Tool Selection

Material Constitutive Model



$$\dot{\epsilon} = \dot{\epsilon}^{\text{el}} + \dot{\epsilon}^{\text{in}} + \dot{\epsilon}^{\text{th}}$$

Ludwik Law ; $\sigma_s = \sigma_y + H\epsilon^n$

Norton-Hoff Law ; $\sigma_{eq} = \sigma_y(T) + H(T)\epsilon^{n(T)} + K(T)(\sqrt{3})^{m(T)+1}\dot{\epsilon}^{m(T)}$

Perzyna Viscoplastic Law

$$\sigma_{eq} = \sigma_y(T) + K(T)(\sqrt{3})^{m(T)+1}\dot{\epsilon}^{m(T)} \epsilon^{n(T)}$$

σ_y : Yield Stress

σ_s : Threshold stress below which no inelastic deformation occurs

H : Strain Dependency

K : Plasticity Consistency

n : Strain Hardening Sensitivity

m : Strain Rate Sensitivity

$$\dot{\epsilon}_{vp} = \left\langle \frac{f(\sigma, q)}{\tau} \right\rangle = \begin{cases} \frac{f(\sigma, q)}{\tau} & \text{if } f(\sigma, q) > 0 \\ 0 & \text{otherwise} \end{cases}$$

1) J.N. Reddy, An Introduction to Continuum Mechanics With Applications, Cambridge University Press, 2008.

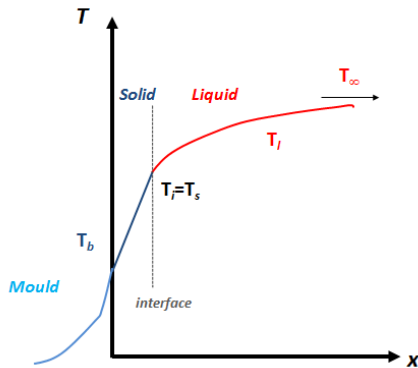
2) P.M. Dixit, U.S. Dixit, Plasticity Fundamentals and Applications, CRC Press, Taylor & Francis Group, 2015.

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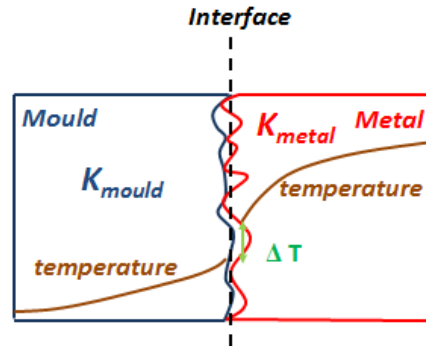
4) O. Heeres, A. Suiker and R. Boster, A comparison between the Perzyna viscoplastic model and the Consistency viscoplastic model, Euro. J. Mech. A-Solid, Vol. 21, 2002, pp. 1-12

Basic Equations in Ingot Casting Simulation-Methodology for Numerical Tool Selection

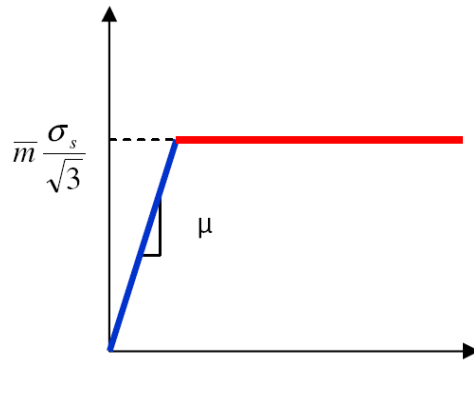
Friction Model



Temperature profile during solidification



Schematic showing the temperature drop due to contact resistance at the interface



➤ Tresca 's Law

$$\tau = \bar{m} \frac{\sigma_{eq}}{\sqrt{3}}$$

➤ Coulomb's Law

$$\tau = \mu \sigma_n$$

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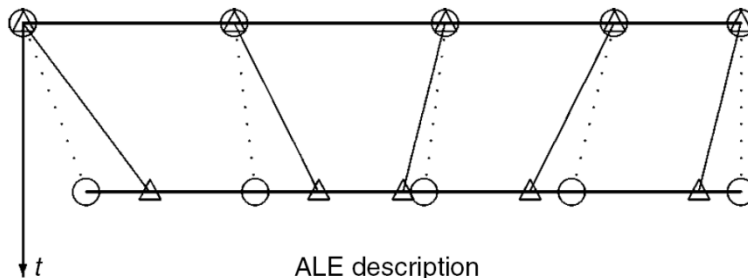
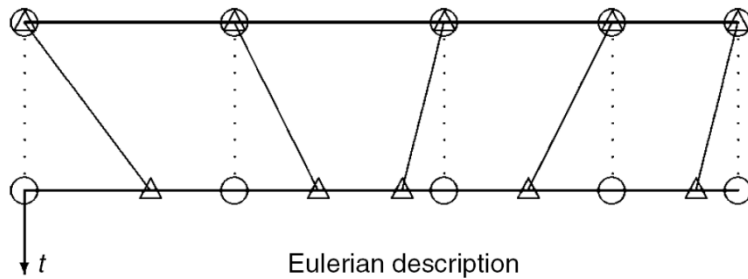
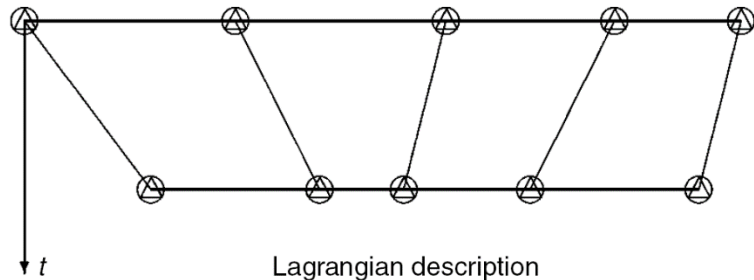
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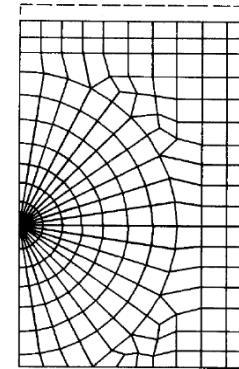
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Basic Equations in Ingot Casting Simulation-Methodology for Numerical Tool Selection

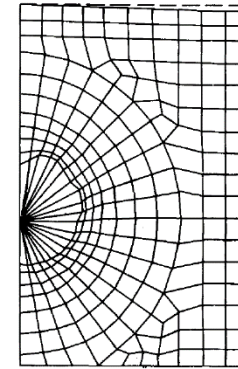
FEM : Algorithms of Continuum Mechanics



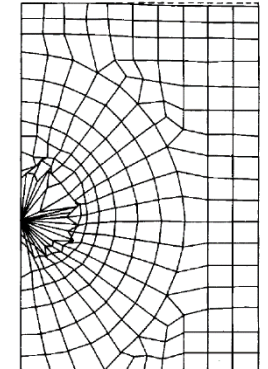
△ Material point ——— Particle motion
○ Node Mesh motion



Initial FE Mesh



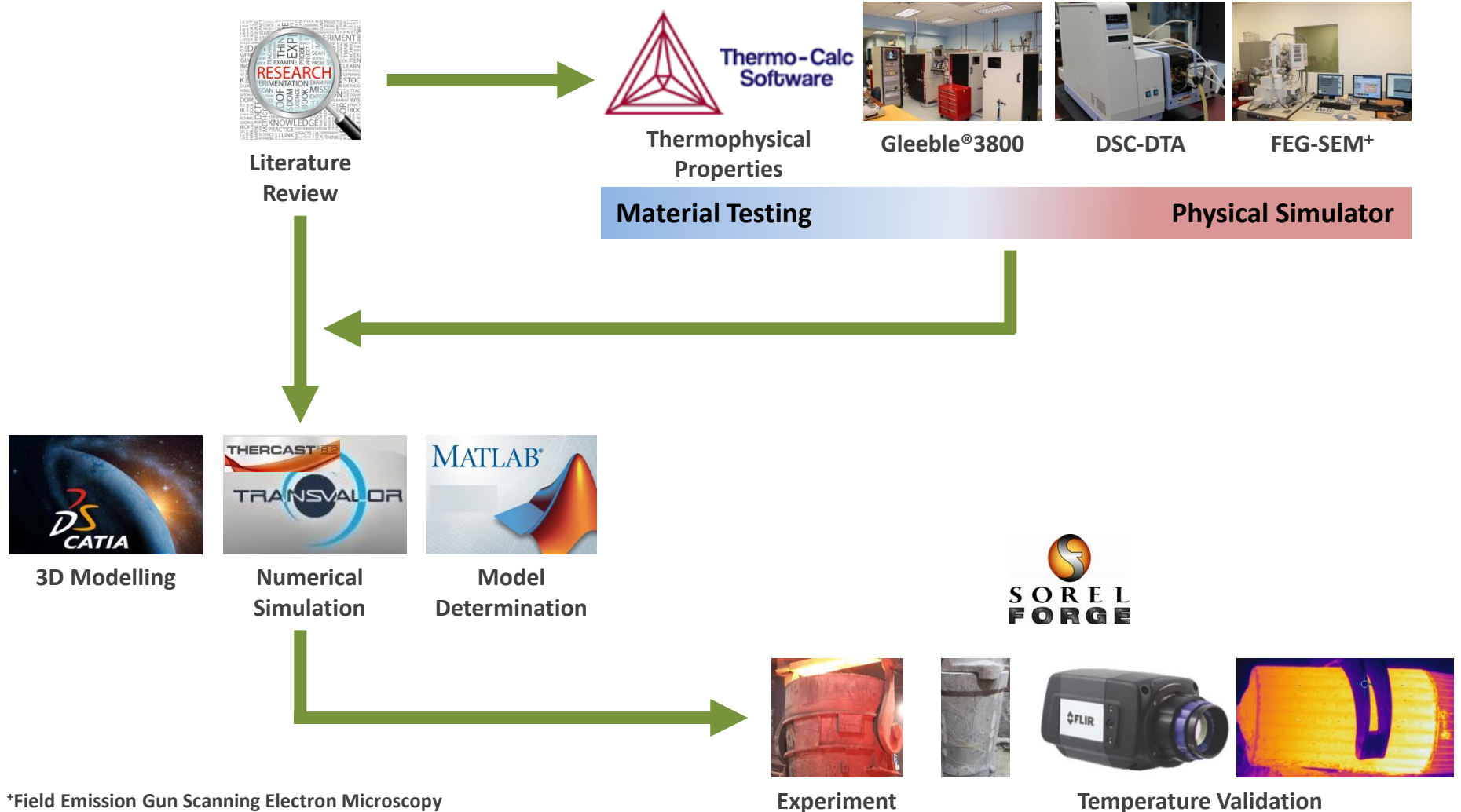
ALE Mesh



Lagrangian Mesh

- ✓ An ALE scheme is used to compute the thermal convection in liquid pool and mushy zone, taking into account the liquid contraction and the solidification shrinkage.
- ✓ The Lagrangian scheme is used to compute the deformation in solid regions, the computational grid is allowed to move with the material: this is essential to treat the air gap between mould and casting.

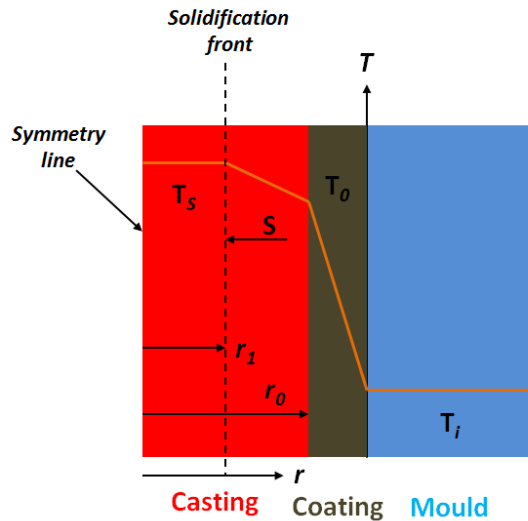
Flow of Steps Involved in the Numerical Modelling and Experimental Verification for of the Large Ingot Solidification



⁺Field Emission Gun Scanning Electron Microscopy

❑ Factors Affecting Solidification

➤ Solidification time in cylindrical case (1D)



$$t = \frac{\rho_c (\Delta H_f + C_p \Delta T)}{2(T_{Solidus} - T_0)} \left[\frac{r_0^2}{K_{mold}} + \frac{r_0}{h_{mold}} \right]$$

ΔH_f [KJ/Kg] : Latent Heat

Mould Temperature (°C)	Pouring Time (min)	Pouring Temperature (°C)
T_M	t_p	T_P

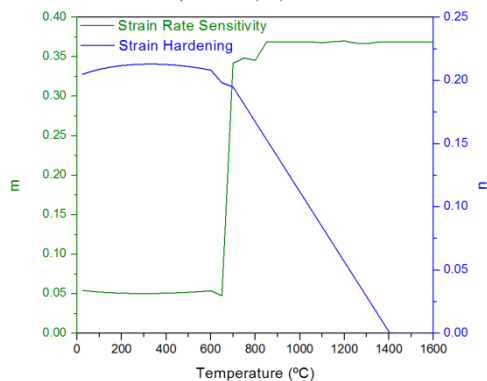
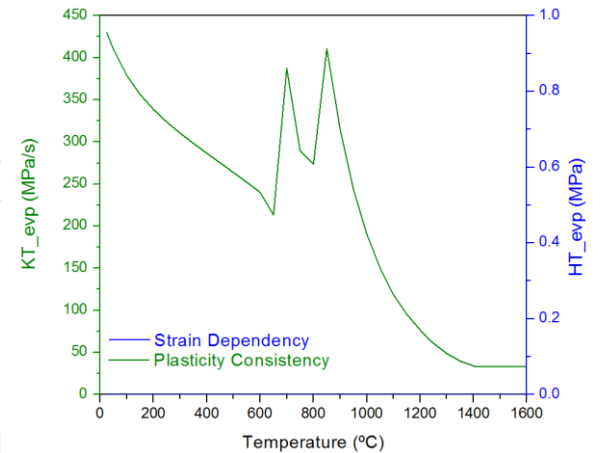
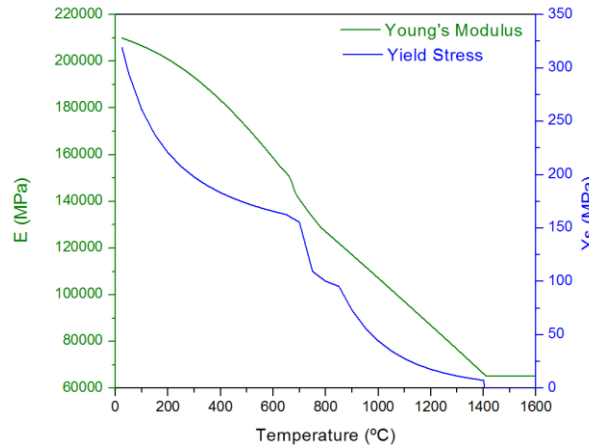
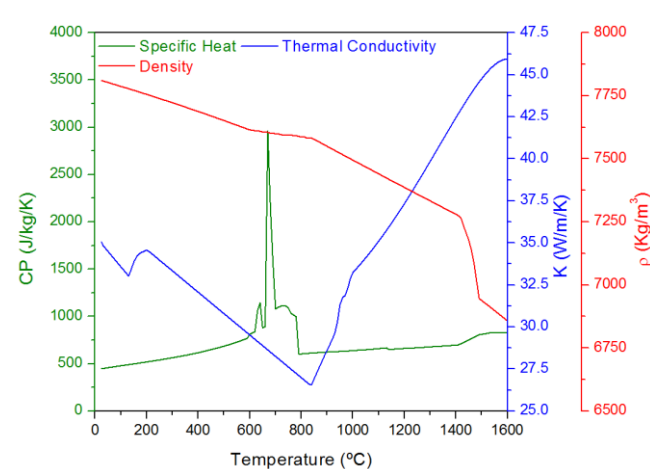
➤ $t_s = f(T_M, t_p, T_P)$

Type of Steel	T_M (°C)	t_p (min)	T_P (°C)
25CrMo4&25-20	150, 350, 550	20, 25, 30	1520, 1545, 1570

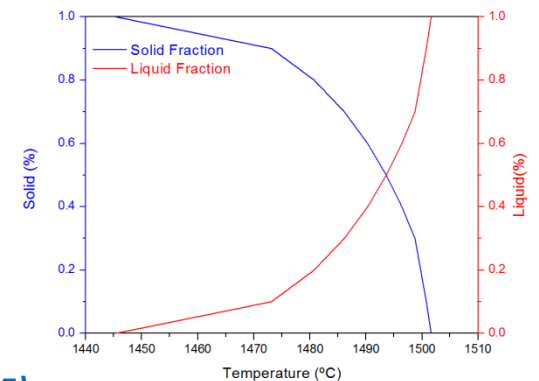
Material Properties

Elements	C	Mn	Ni	Cr	Mo	Cu	Si	S	P
25CrMo4 Comp.(wt.%)	0.25	0.9	0.3	1.2	0.3	0.3	0.4	0.02	0.035
25-20 Comp.(wt.%)	0.08	0.79	20	25	5	1.8	0.075	0.015	0.04

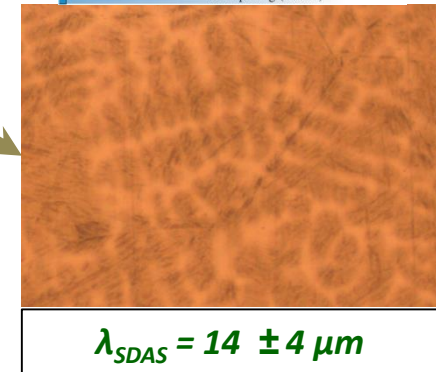
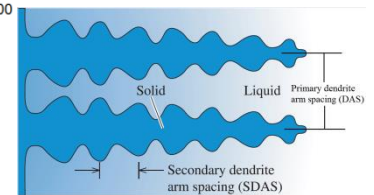
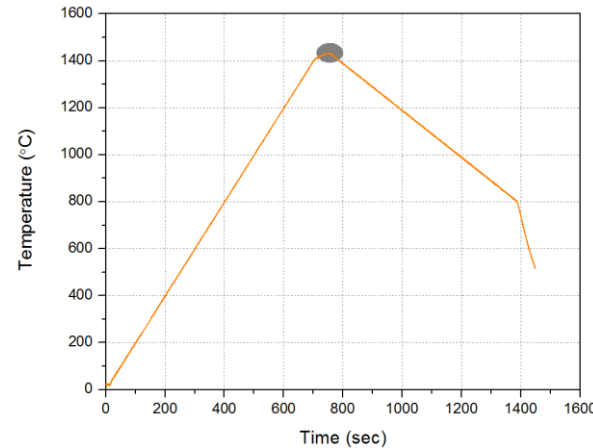
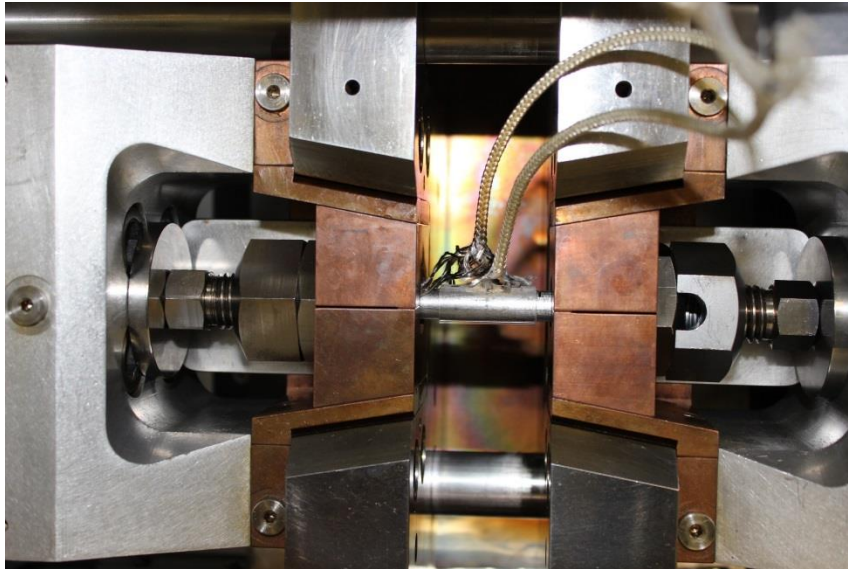
➤ 25CrMo4



	25CrMo4	25-20
Emissivity	0.8	0.8
Poisson Coefficient	0.3	0.3
Solidification Shrinkage Factor	-0.0385	-0.03
Latent Heat (KJ/Kg)	265	309



Material Properties-Material Testing & Physical Simulator

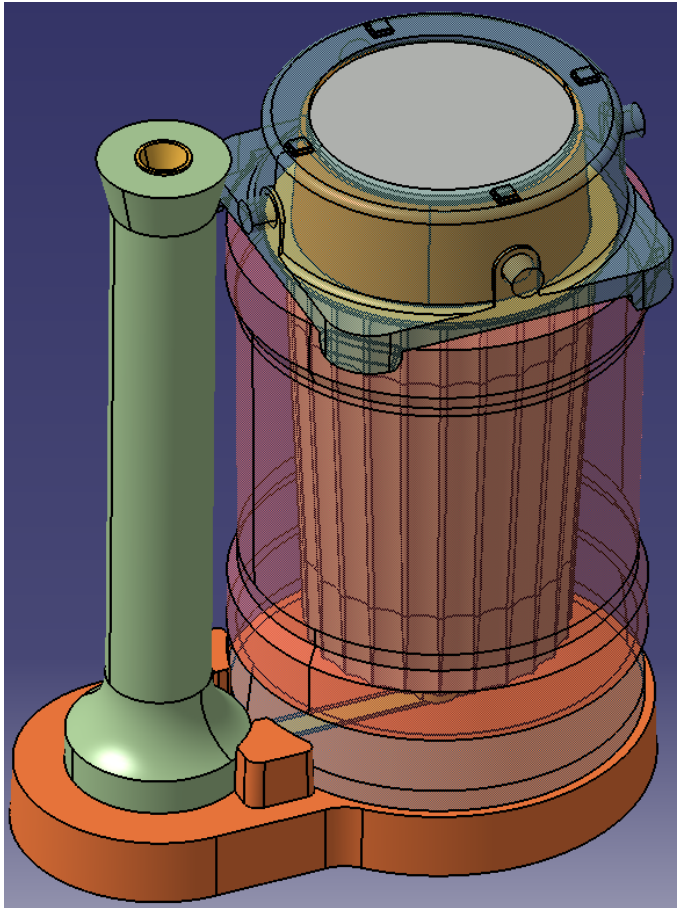


The characteristic terms of a dendrite: primary and secondary dendrite arm spacing

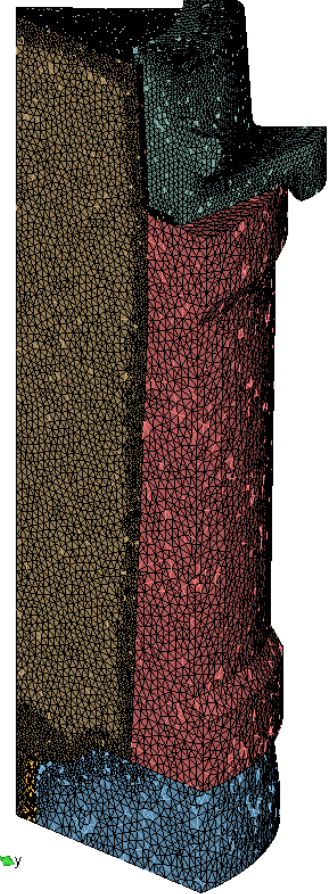
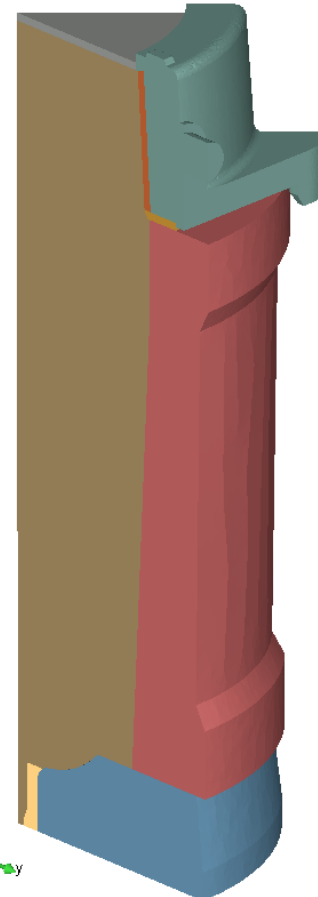
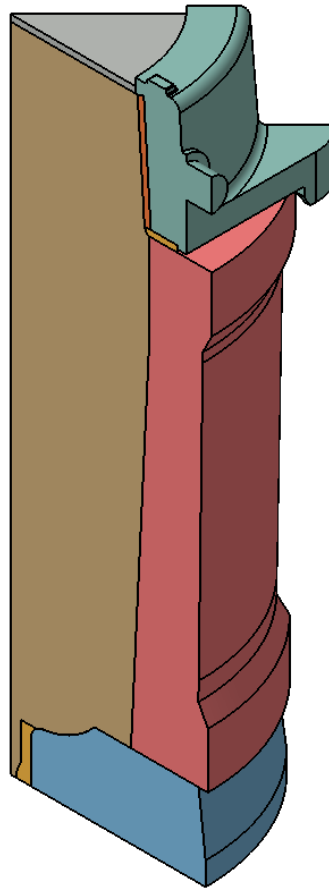


□ Geometrical Modelling and Computational Mesh Generation

➤ 40 MT Ingot



3D Geometrical Models in Catia



3D Computational Mesh in Thercast

❑ Setup Numerical Simulation on CLUMEQ

- The CLUMEQ High Performance Computing Center at ÉTS
- ✓ Top 35 worldwide
- ✓ 5,000 square-feet of IT space and 5 PB of attached parallel storage at ÉTS with 1570 nodes (20400 cores) IBM cluster
- ✓ Compute Partitions: High Bandwidth(400nodes), Large Memory (346 nodes) and Serial Workload(824 nodes) .



□ Empirical Model for Solidification Time

- A first-order response surface model is:

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3 + \epsilon$$

- A second-order model is usually obtained by adding quadratic terms:

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3 + \beta_{11} x_1^2 + \beta_{22} x_2^2 + \beta_{33} x_3^2 + \beta_{12} x_1 x_2 + \beta_{13} x_1 x_3 + \beta_{23} x_2 x_3 + \epsilon$$

$$\therefore \hat{y} = y - \epsilon$$

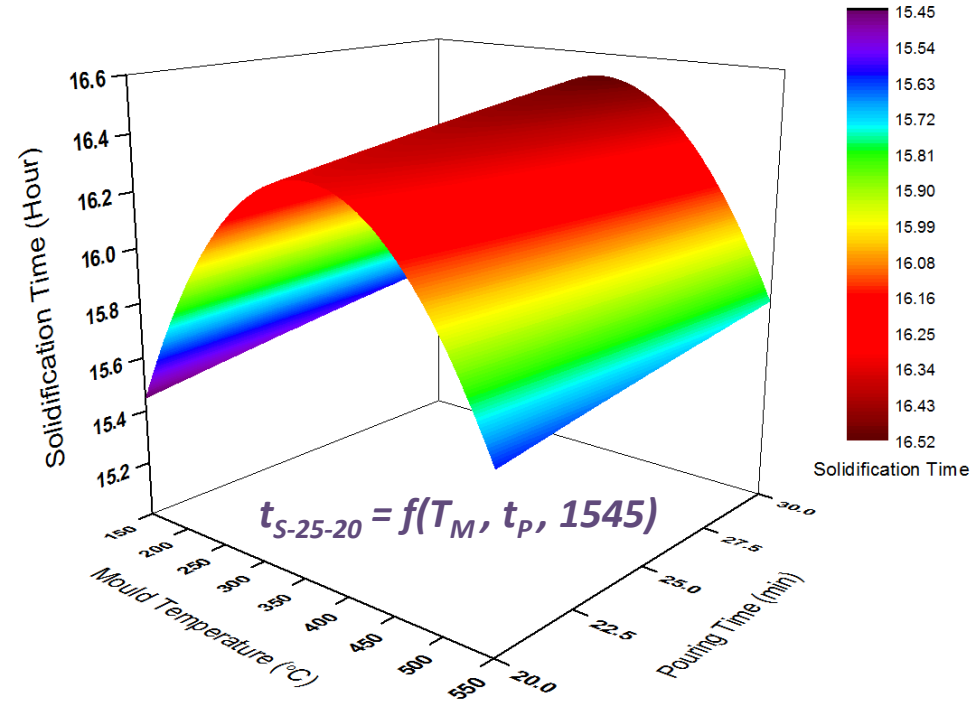
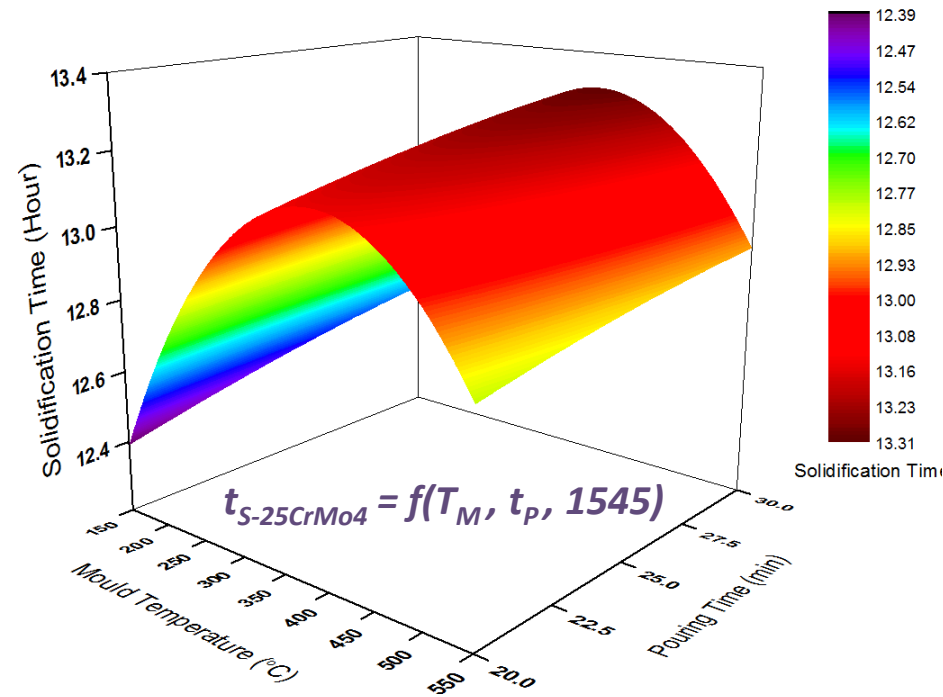
- ✓ The actual response model, $\hat{y}$, based on the observations of y_i , from 27 simulation results for each material, may be expressed as:

$$\hat{y} = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3 + \beta_{11} x_1^2 + \beta_{22} x_2^2 + \beta_{33} x_3^2 + \beta_{12} x_1 x_2 + \beta_{13} x_1 x_3 + \beta_{23} x_2 x_3$$

Results and Discussion

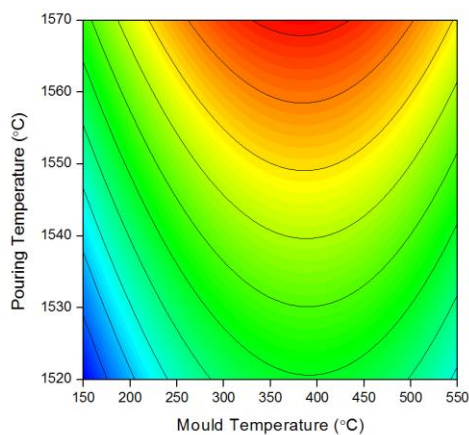
➤ 25CrMo4

➤ 25-20

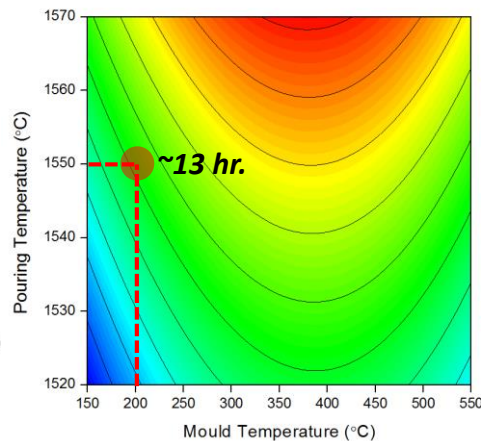


Results and Discussion

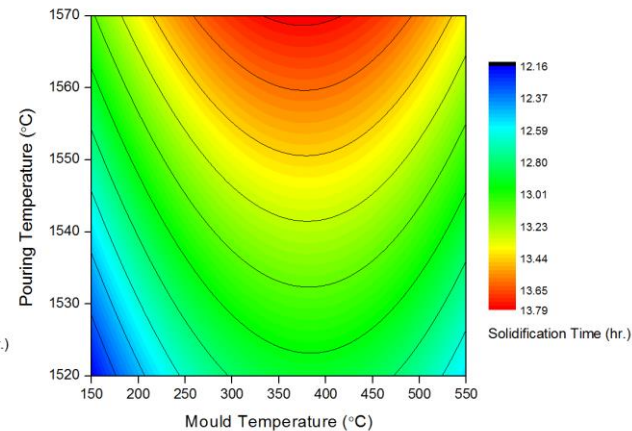
25CrMo4



$$t_{S-25CrMo4} = f(T_M, 20, T_P)$$

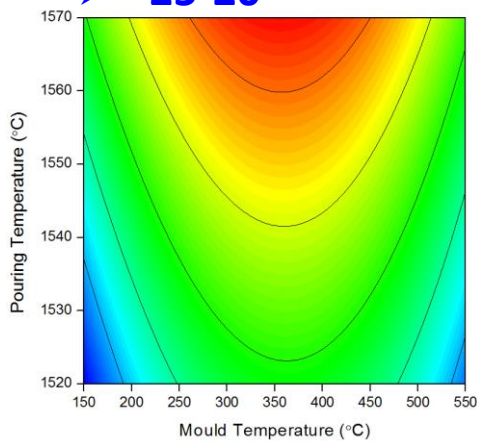


$$t_{S-25CrMo4} = f(T_M, 25, T_P)$$

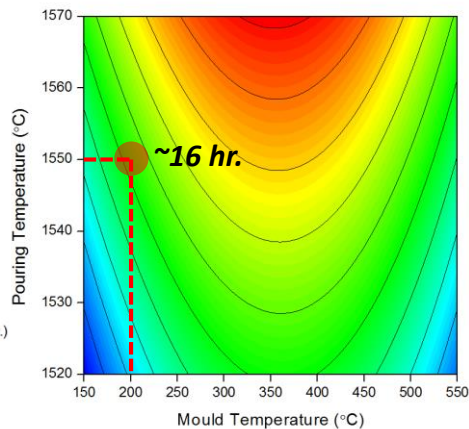


$$t_{S-25CrMo4} = f(T_M, 30, T_P)$$

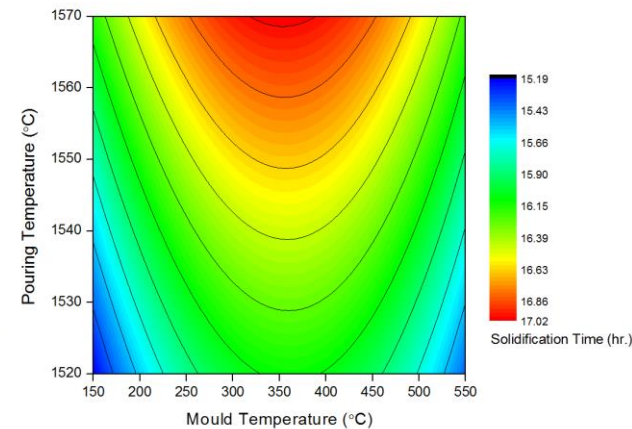
25-20



$$t_{S-25-20} = f(T_M, 20, T_P)$$



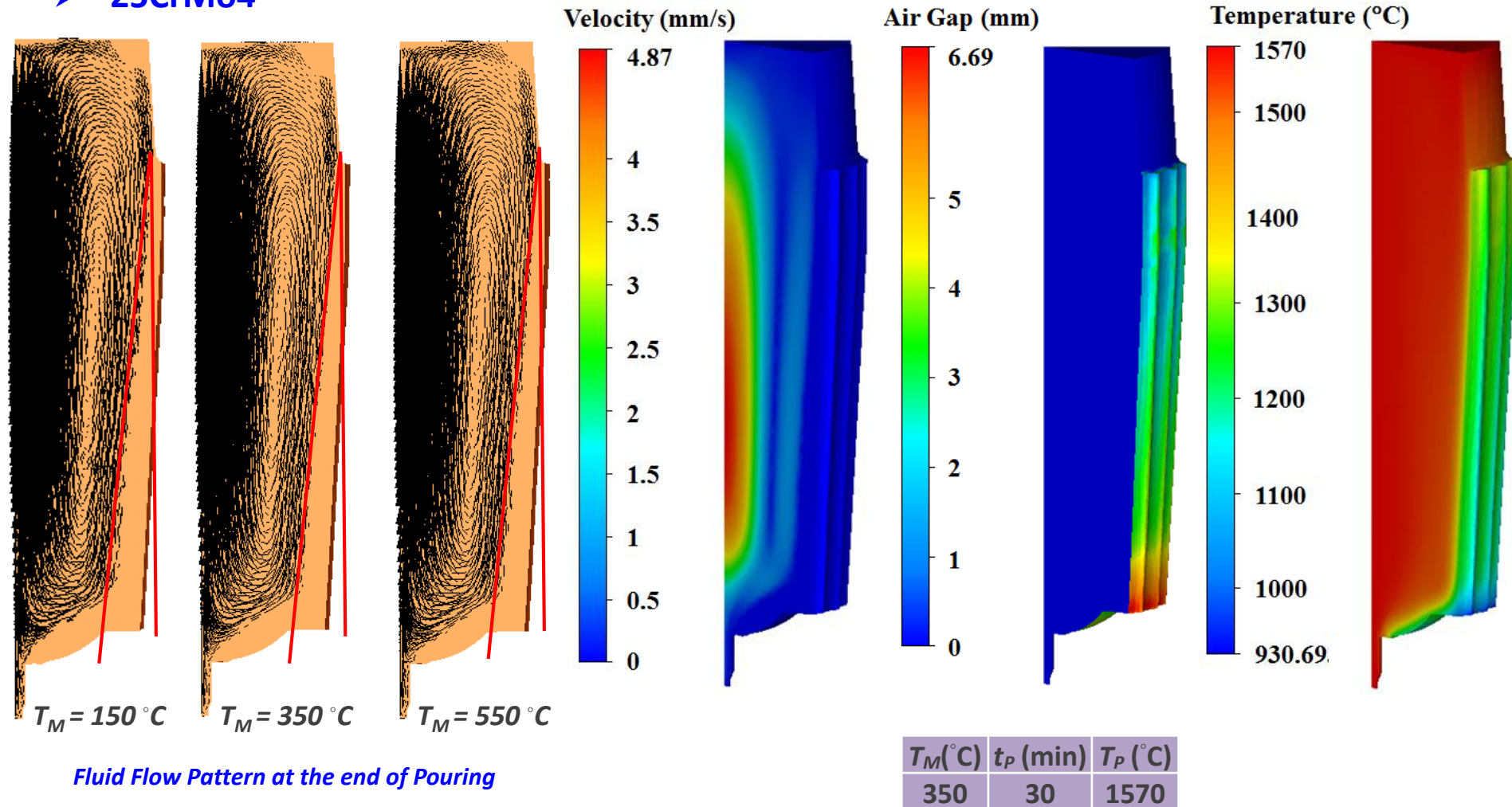
$$t_{S-25-20} = f(T_M, 25, T_P)$$



$$t_{S-25-20} = f(T_M, 30, T_P)$$

Results and Discussion

25CrMo4

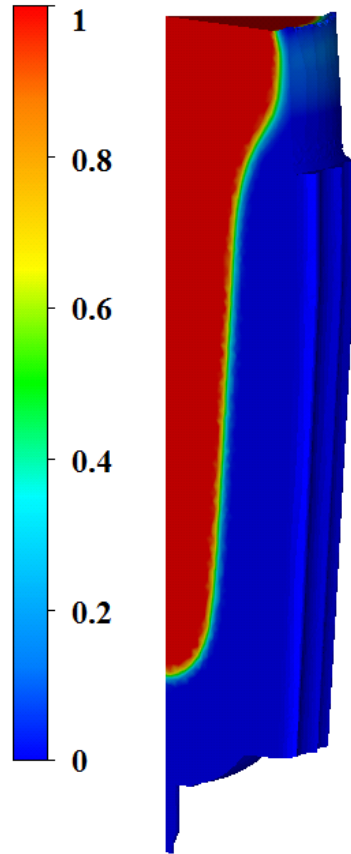


Velocity, Air Gap and Temperature Patterns at the end of Pouring

Results and Discussion

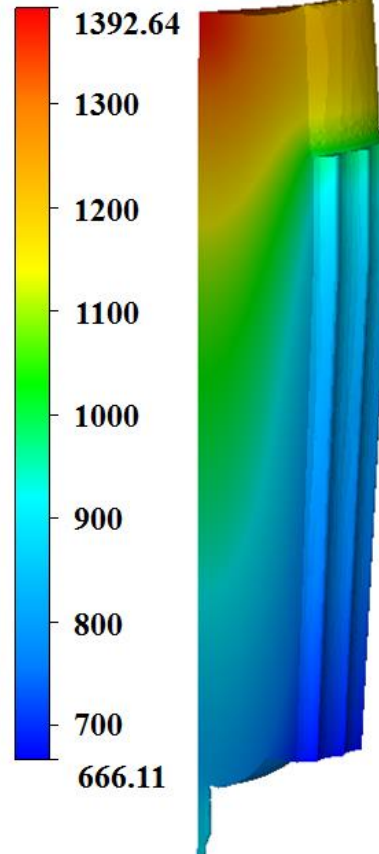
➤ 25CrMo4

Liquid Fraction (%)



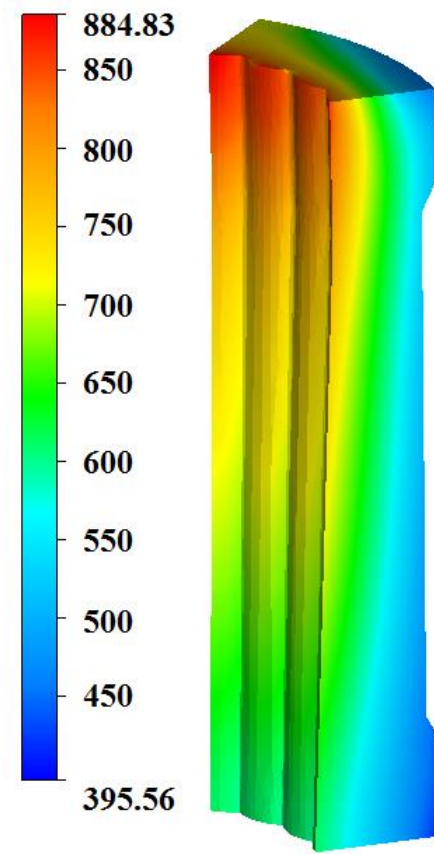
after 50% Solidification

Temperature (°C)

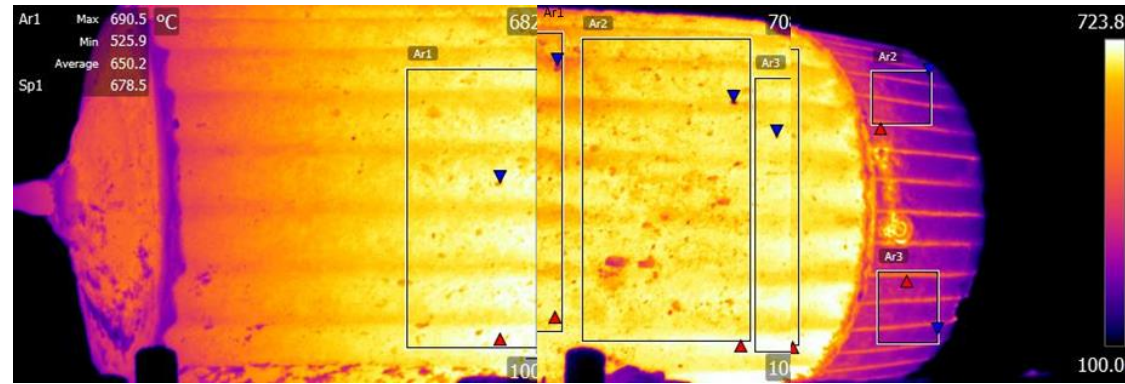
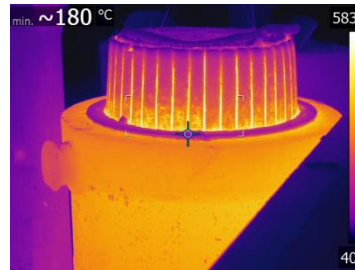


Ingot & Mould Temperature Patterns after 100% Solidification

Temperature (°C)

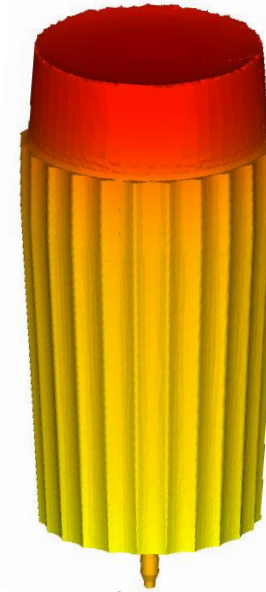
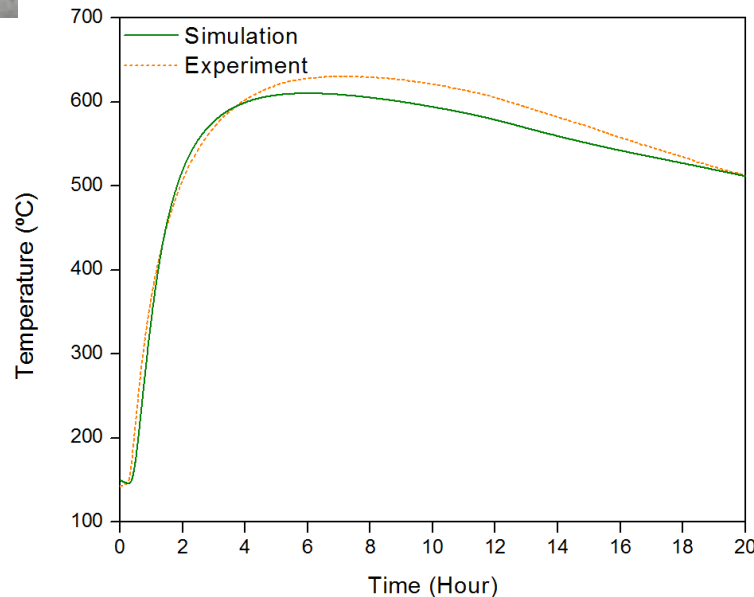


Experimental Validation



Infrared Radiation Thermography Camera

Thermocouples data
Recording



❑ Conclusions

- ✓ The effect of critical process parameters on the solidification behaviour of two different steels were studied.
- ✓ The predictive models for the solidification time of the two steels were obtained.
- ✓ The obtained results were validated against actual experimental data and showed very good agreement.
- ❖ Mathematical models are used for proper selection of ingot casting parameters.

➤ Acknowledgments



Thanks for Your Attention

➤ *Any Question?*